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Effect of drift layer doping and NiO parameters in achieving 8.9 kV breakdown in 100 μm diameter and 4 kV/4 A in 1 mm diameter NiO/ $\beta\text{-Ga}_2\text{O}_3$ rectifiers

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Effect of drift layer doping and NiO parameters in achieving 8.9 kV breakdown in 100 μm diameter and 4 kV/4 A in 1 mm diameter NiO/ $\beta\text{-Ga}_2\text{O}_3$ rectifiers

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ABSTRACT

The effect of doping in the drift layer and the thickness and extent of extension beyond the cathode contact of a NiO bilayer in vertical NiO/ $\beta\text{-Ga}_2\text{O}_3$ rectifiers is reported. Decreasing the drift layer doping from 8×10^{15} to $6.7 \times 10^{15} \text{ cm}^{-3}$ produced an increase in reverse breakdown voltage (V_B) from 7.7 to 8.9 kV, the highest reported to date for small diameter devices (100 μm). Increasing the bottom NiO layer from 10 to 20 nm did not affect the forward current–voltage characteristics but did reduce reverse leakage current for wider guard rings and reduced the reverse recovery switching time. The NiO extension beyond the cathode metal to form guard rings had only a slight effect (~5%) in reverse breakdown voltage. The use of NiO to form a pn heterojunction made a huge improvement in V_B compared to conventional Schottky rectifiers, where the breakdown voltage was ~1 kV. The on-state resistance (R_{ON}) was increased from $7.1 \text{ m}\Omega \text{ cm}^2$ in Schottky rectifiers fabricated on the same wafer to $7.9 \text{ m}\Omega \text{ cm}^2$ in heterojunctions. The maximum power figure of merit (V_B)²/ R_{ON} was 10.2 GW cm^{-2} for the 100 μm NiO/ Ga_2O_3 devices. We also fabricated large area (1 mm²) devices on the same wafer, achieving V_B of 4 kV and 4.1 A forward current. The figure-of-merit was 9 GW cm^{-2} for these devices. These parameters are the highest reported for large area Ga_2O_3 rectifiers. Both the small area and large area devices have performance exceeding the unipolar power device performance of both SiC and GaN.

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I. INTRODUCTION

The increasing electrification of automobiles and the need to switch renewable energy sources in the existing power grid has increased demand for energy efficient power electronics capable of higher voltage and currents than existing Si devices. This has focused attention on the wide and ultra-wide bandgap semiconductors,^{1–5} with the latter including diamond, AlN, and Ga_2O_3 . The ability to grow large diameter, high quality crystals from melt-grown methods and the attendant low cost of production has spurred interest in $\beta\text{-Ga}_2\text{O}_3$.^{1–5} One of the goals is to achieve a high-power figure of merit for power electronic devices, defined as (V_B)²/ R_{ON} where V_B is the reverse breakdown voltage and R_{ON} is the on-state resistance.^{1,3,4}

To achieve a high-power figure of merit, a rectifier must have a low drift layer concentration, with high electron mobility, as well as low R_{ON} , and optimized edge termination to prevent current crowding.^{1,5–21} The breakdown voltage is larger for thicker drift layers, but this degrades on-resistance. To achieve a low R_{ON} , a thin drift layer with high electron mobility is required. In addition, vertical geometry devices are desirable, because of their higher power conversion efficiency and absolute currents compared to lateral devices.^{1,3–5} Power rectifiers are also building blocks for many advanced power handling systems.

A drawback with Ga_2O_3 is the absence of facile p-type doping. All of the potential acceptor dopants have large ionization energies

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and are not significantly ionized at room temperature. This has led to the use of p-type oxides, principally polycrystalline NiO, to form p-n heterojunctions with n-type Ga₂O₃.^{6–14} The forward current transport mechanism in such junctions is typically recombination at low biases and trap-assisted tunneling at higher bias.^{10,21–26} Promising rectifier performance has been reported with this approach,^{12–14,21–39} including V_B of 8.32 kV, with figure of merit of 13.2 GW cm⁻².¹²

Optimization of the heterojunction rectifier device structure is crucial to achieve both high V_B and low R_{ON}, as well as providing management of the maximum electric fields within the structure to enhance further the device voltage blocking capability.^{40–46} The design variables include the thickness and doping of the layers, doping in the drift layer and the use of the NiO as a guard ring by extending it beyond the metal cathode. In this paper, we report an investigation of the effect of these parameters on the performance of NiO/Ga₂O₃ vertical rectifiers. A new highest V_B for these devices is achieved.

II. EXPERIMENT

We made both vertical geometry Schottky rectifiers and NiO/Ga₂O₃ rectifiers on the same wafers. The parameters investigated are shown in the schematic of the vertical heterojunction rectifiers in Fig. 1. We varied the thickness of the second layer in the bilayer NiO (10 or 20 nm, with fixed thickness of the top layer held constant at 10 nm) and the length of the NiO extension beyond the cathode contact (12–20 μm) to form guard rings. The choice of these parameters was guided by TCAD simulations with the Silvaco Atlas code of electric field distributions, as reported previously.¹⁴ Finally, we had two different drift region doping levels at a fixed thickness of 10 μm. The epitaxial layers were grown by halide vapor phase epitaxy (HVPE) on a (001) Sn-doped (10¹⁹ cm⁻³)

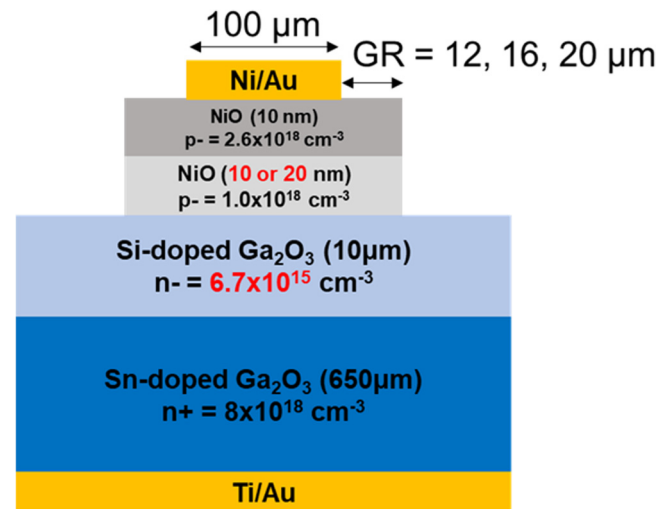


FIG. 1. Schematic of the NiO/Ga₂O₃ heterojunction rectifier. The extension of NiO beyond the Ni/Au contact to act as a guard ring was investigated for different extension lengths, as well as the thickness of the bottom NiO layer and the drift layer doping.

β-Ga₂O₃ single crystal substrate. These samples were purchased from Novel Crystal Technology, Japan.

Ohmic contacts were made to the rear surface using a Ti/Au metal stack deposited by e-beam evaporation. This was annealed at 550 °C for 180 s under N₂. The front surface was exposed to UV/ozone exposure for 15 min to remove contamination. The NiO bilayer was deposited by rf (13.56 MHz) magnetron sputtering at a working pressure of 3 mTorr.^{14,40} The hole concentration in these films was adjusted using the Ar/O₂ ratio. The structure was then annealed at 300 °C under O₂. Finally, a cathode contact of 20/80 nm Ni/Au (100 μm diameter) was deposited onto the NiO layer. The NiO was extended from 12 to 20 μm beyond the contact metal to form a guard ring. Figure 2 shows the C⁻²-V plots for the two different drift layer doping levels. These show the carrier concentrations were 6.7 × 10¹⁵ and 8 × 10¹⁵ cm⁻³, respectively.

The current density–voltage (J–V) characteristics were measured on a Tektronix 370-A curve tracer, 371-B curve and Agilent 4156C. For the highest reverse voltages, a Glassman power supply was employed. The reverse breakdown voltage was defined as the bias for a reverse current reaching 0.1 A·cm⁻². The high bias measurements were performed in Fluorinert atmosphere at 25 °C. The devices did not suffer permanent damage at this condition but increasing the voltage a further 50–200 V led to permanent failure through breakdown at the contact periphery. The on-resistance values were calculated assuming the current spreading length is 10 μm and a 45° spreading angle. We also subtracted the resistance of the cable, probe, and chuck, which was around 10 Ω.

III. RESULTS AND DISCUSSION

A. Small area rectifiers to achieve high breakdown voltage

Figure 3 shows the forward current densities and R_{ON} values for rectifiers with different guard ring dimensions fabricated with

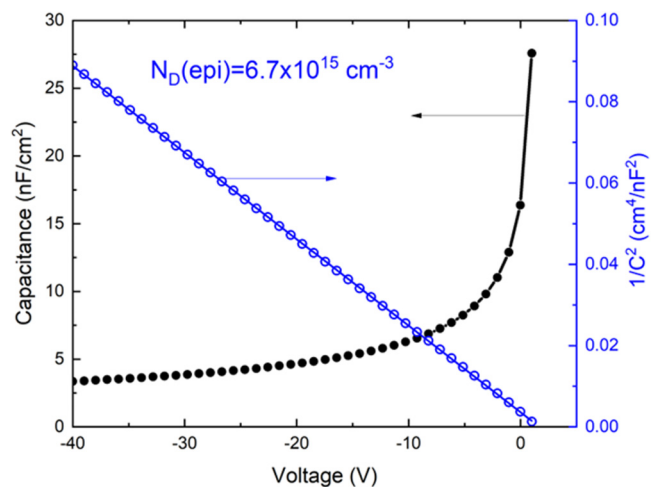


FIG. 2. C–V characteristics for determining carrier density in the drift region for the two different types of wafers investigated. The drift layer thickness was ~10 μm in both cases.

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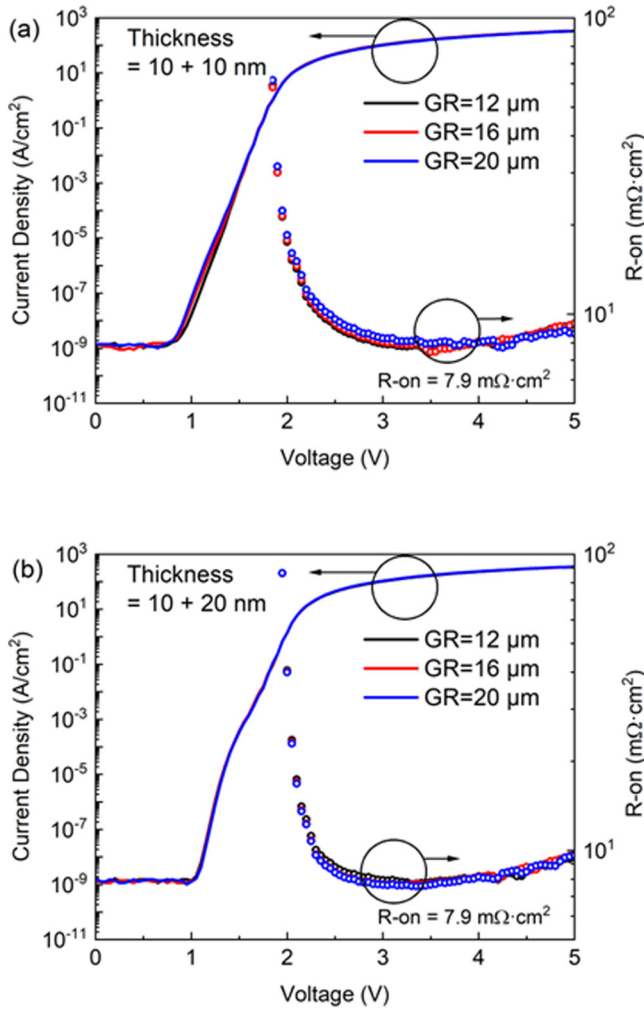


FIG. 3. Forward current densities and R_{ON} values for rectifiers with different guard ring dimensions fabricated with (a) 10/10 nm NiO bilayer or (b) 10/20 nm NiO bilayer.

(a) 10/10 nm NiO bilayer or (b) 10/20 nm NiO bilayer. These were fabricated on the drift region with the lower carrier density. There is very little difference in these forward current density characteristics for either the NO bilayer thickness or the guard ring diameter.

Figure 4 shows a comparison of the results from the NiO/Ga₂O₃ heterojunction rectifiers with the Schottky rectifier fabricated on the same wafer. The on-resistance for the former was 7.9 mΩ cm⁻². For the Schottky rectifiers, this parameter was slightly lower, as expected, at 7.1 mΩ cm⁻². Both types of devices had forward current densities >100 A cm⁻² at 5 V. The turn-on voltage was 1.9–2.1 V for the heterojunction rectifiers.

Figure 5 shows the reverse I–V characteristics out to –100 V for (a) NiO/Ga₂O₃ rectifiers with 10/10 nm NiO bilayers or (b) 10/20 nm NiO bilayers. While the guard ring diameter makes little

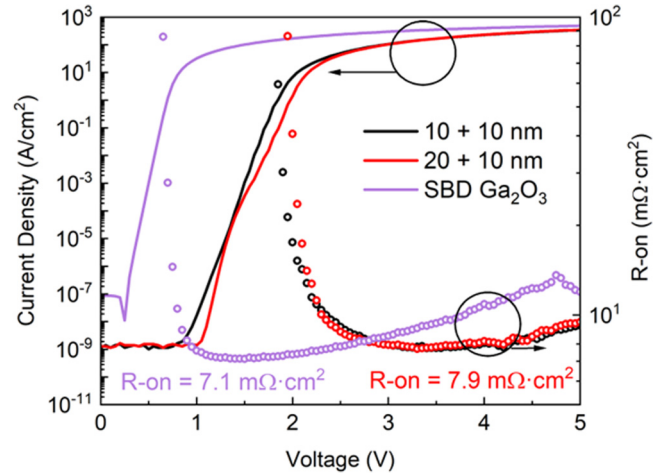


FIG. 4. Comparison of forward current density characteristics for Schottky and NiO/Ga₂O₃ rectifiers.

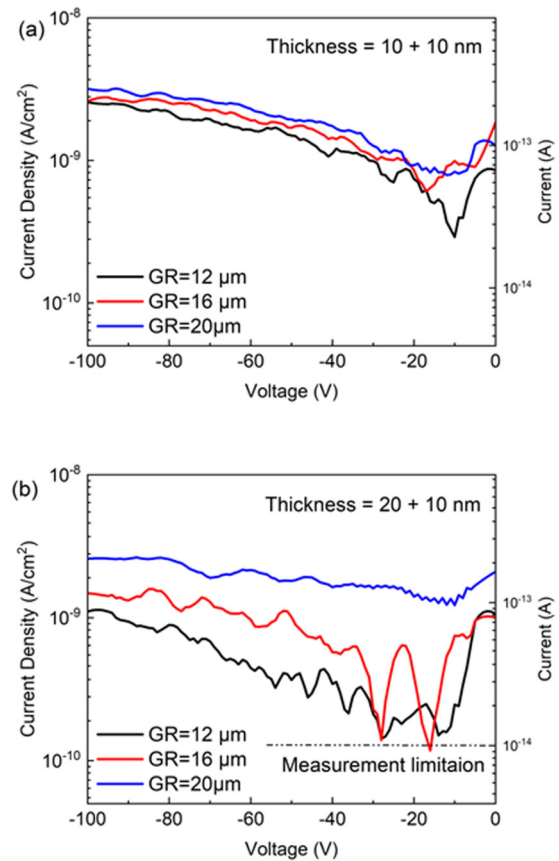


FIG. 5. Reverse I–V characteristics out to –100 V for (a) NiO/Ga₂O₃ rectifiers with 10/10 nm NiO bilayers or (b) 10/20 nm NiO bilayers.

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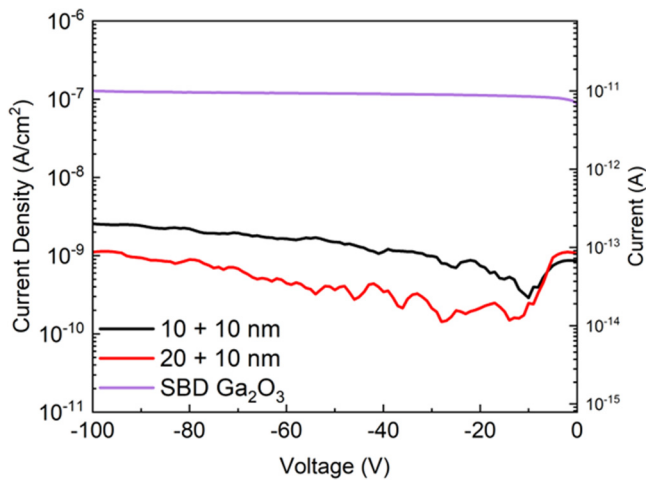


FIG. 6. Comparison of low bias reverse current characteristics between Schottky rectifiers and NiO/Ga₂O₃ rectifiers with either 10/10 nm or 10/20 nm bilayers. All these were fabricated on the sample with drift layer doping of $6.7 \times 10^{15} \text{ cm}^{-3}$.

difference to devices with the 10/10 nm NiO bilayer, there is a reduction in reverse current density for the smaller guard rings. A comparison of the heterojunction results with those from the Schottky rectifiers all fabricated on the lower drift layer doping structure is shown in Fig. 6 for a fixed guard ring diameter of $12 \mu\text{m}$ in the latter type of device. As expected, the leakage current from the heterojunction rectifiers is lower than that of the Schottky rectifier and reducing the doping in the drift layer also lowers the reverse current density.^{20,21,47–50} Similar trends were observed for the two types of devices fabricated on the higher drift layer doping. The p-n junction has a larger effective barrier for current transport than the metal gate Schottky rectifiers.

The reverse J-V characteristics over the full bias range are shown in Fig. 7(a) for the devices fabricated on the $6.7 \times 10^{15} \text{ cm}^{-3}$ drift layers with different NiO thicknesses as well as different guard ring diameters. Once again, for comparison, we show the result for the Schottky rectifier and for a heterojunction device fabricated on the wafer with larger drift layer concentration of $8 \times 10^{15} \text{ cm}^{-3}$. The key points from these data are first, that the lower doping produces a higher reverse breakdown voltage, with a maximum of 8.9 kV. This is the highest reported to date for Ga₂O₃ rectifiers of any type.¹² The second point is that the heterojunction really increases reverse breakdown voltage compared to the Schottky rectifier. V_b of the latter was 750 V, while the device reached 1218 V before permanent burn out. The final point is that the NiO thickness and guard ring extension length made only a relatively small difference in V_b .

Figure 7(b) shows a comparison of the breakdown voltages for the devices fabricated on the lower drift layer doped layers, as a function of the NiO thickness. The power figure of merit was 10.2 GW cm^{-2} for the optimized heterojunction rectifier, compared to 0.08 GW cm^{-2} for the Schottky rectifier. The theoretical

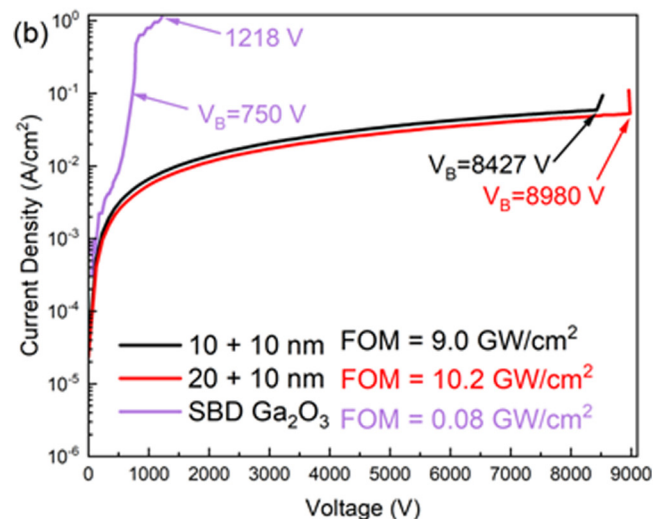
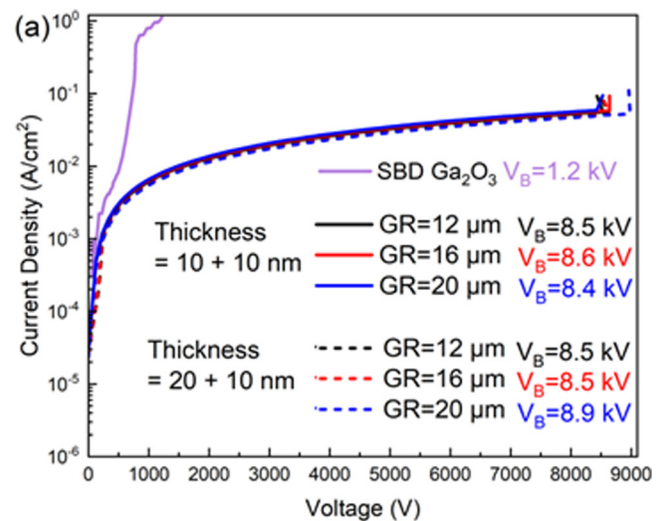


FIG. 7. (a) Reverse current characteristics from the Schottky rectifier and NiO/Ga₂O₃ heterojunction rectifiers with different guard ring extensions and NiO layer thicknesses. (b) Comparison between Schottky and NiO/Ga₂O₃ heterojunction rectifiers fabricated on the lowest drift layer doping wafer.

maximum is $\sim 34 \text{ GW cm}^{-2}$, showing that further improvement should be possible as the edge termination and epi layer quality continue to evolve.^{4,12} The average electric field strength is 8.7 MV/cm . For biases $>100 \text{ V}$, the reverse leakage current follows a $\ln(I) \propto V$ relation. This indicates the dominant leakage mechanism is electron variable-range-hopping via defect-related states in the drift region.^{9,10,12,14} This has been reported in detail by numerous groups.

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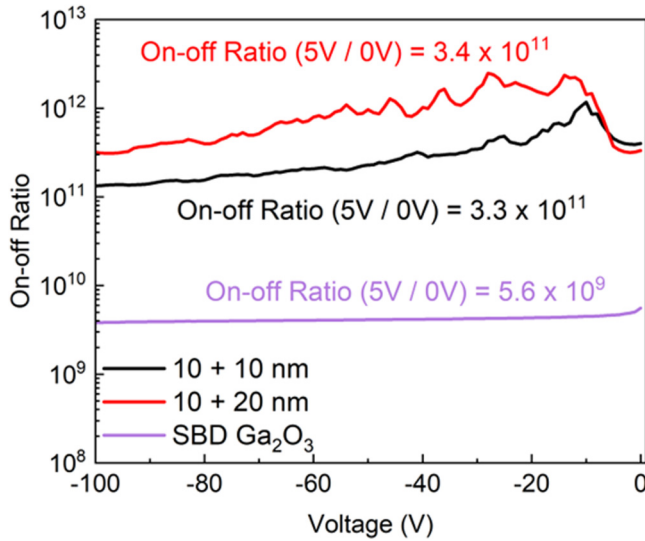


FIG. 8. On-off ratio of 100 μm diameter NiO/Ga₂O₃ heterojunction rectifiers in which the bias was switched from 5 V forward to the voltage shown on the x axis. For comparison, the results for a Schottky rectifier fabricated on the same wafer are included.

Figure 8 shows the on-off ratio of NiO/Ga₂O₃ heterojunction rectifiers in which the bias was switched from 5 V forward to the reverse voltage shown on the x axis. For comparison, the results for a Schottky rectifier fabricated on the same wafer are included. The values are still $>10^{11}$ when switching to 100 V and approximately two orders of magnitude higher than that of the Schottky rectifier over this bias range. This again emphasizes an advantage of the p-n heterojunction in achieving excellent rectification characteristics.

Figure 9 shows the reverse recovery switching waveform when switching from 50 mA forward current to -10 V for heterojunction rectifiers with (a) 10/10 nm or (b) 10/20 nm bilayers as a function of guard ring extension. The reverse recovery times are ~ 21 ns and are tabulated in Table I. These measurements were made with a custom switching circuit, as described previously.^{40–42} We used di/dt values around 2.9 A/ μs . Others have reported use of values in the range 100–400 A/ μs .^{47,51} Figure 10 shows a comparison of switching waveforms of Schottky and NiO/Ga₂O₃ heterojunction rectifiers. The relative indifference to device structure demonstrates that charge storage in the p-n junction is not a significant factor compared to the Schottky device.^{13,14} The Schottky diode had higher forward current due to lower effective barrier height.

Figure 11 shows a literature compilation of Ron versus V_B results for all the common types of rectifiers fabricated in the Ga₂O₃ materials system. These include metal gate Schottky barrier or junction barrier Schottky rectifiers, along with NiO/Ga₂O₃ heterojunction rectifiers. This is a standard chart for showing the improvement in Ga₂O₃ rectifier performance and contains the theoretical lines for SiC, GaN, and Ga₂O₃ devices. Note that there are now at least five instances of Ga₂O₃ rectifiers with performance beyond the one-dimensional unipolar limits of GaN and SiC. It is

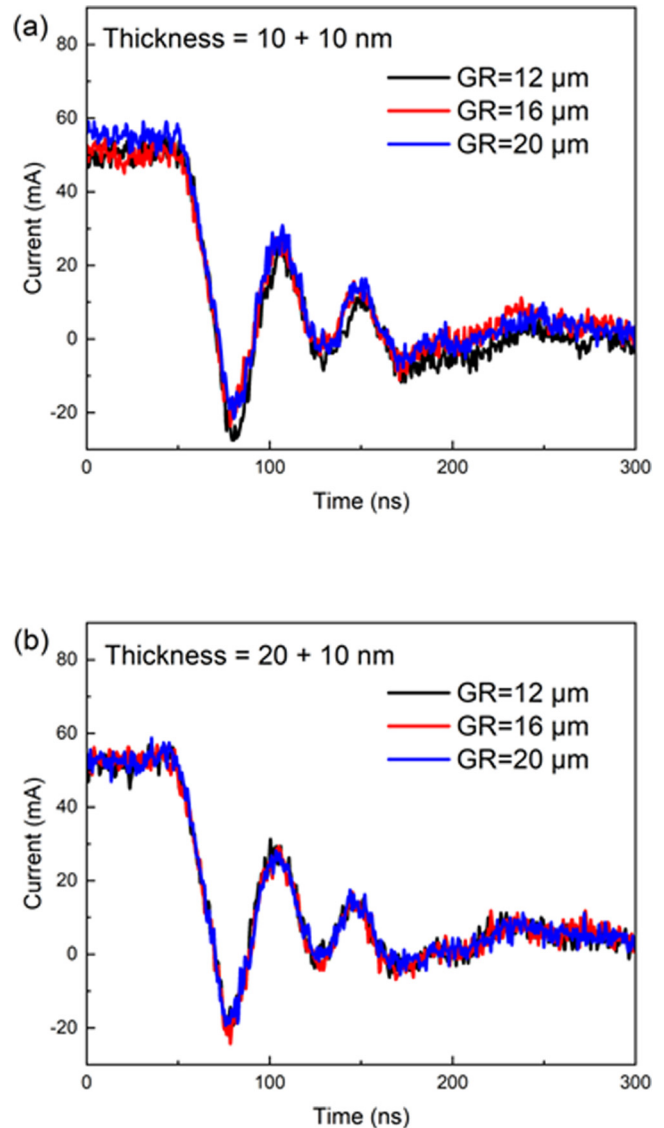


FIG. 9. (a) Switching waveform for NiO/Ga₂O₃ heterojunction rectifiers with (a) 10/10 nm or (b) 10/20 nm bilayers as a function of guard ring extension.

expected that continued optimization of the edge termination techniques and reductions in both drift layer doping and defect density should advance the ability to make large area rectifiers with high conduction currents using the NiO/Ga₂O₃ structures. The reliability of such structures will also need to be investigated.^{52–54}

B. Large area devices to achieve high forward current

There has been much less reported on large area Ga₂O₃ rectifiers, which are needed to achieve large absolute forward conduction currents.^{46,51,55–63} These are typically referred to as

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TABLE I. Summary of reverse recovery parameters for heterojunction and Schottky rectifiers.

	T_{rr} (ns)	I_{rr} (mA)	dI/dT (A/ μ s)	I_F (mA)
10 + 10 nm	19.6	27.5	2.9	50
20 + 10 nm	13.8	21.6	2.9	50
Schottky	14.6	21.4	2.5	65

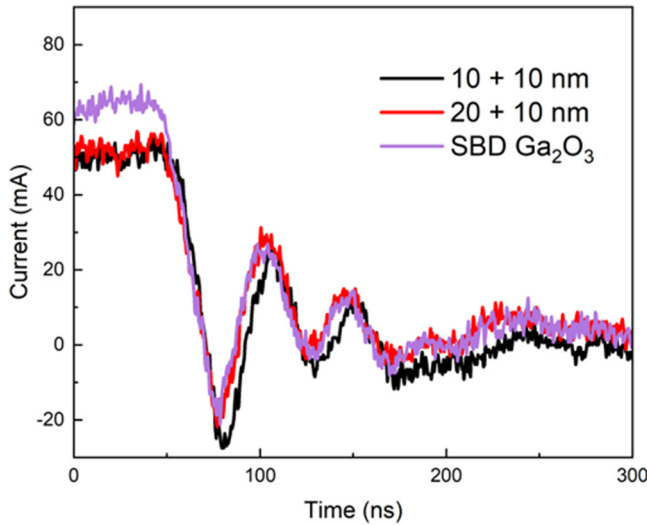


FIG. 10. Comparison of switching waveforms of Schottky and NiO/Ga₂O₃ heterojunction rectifiers.

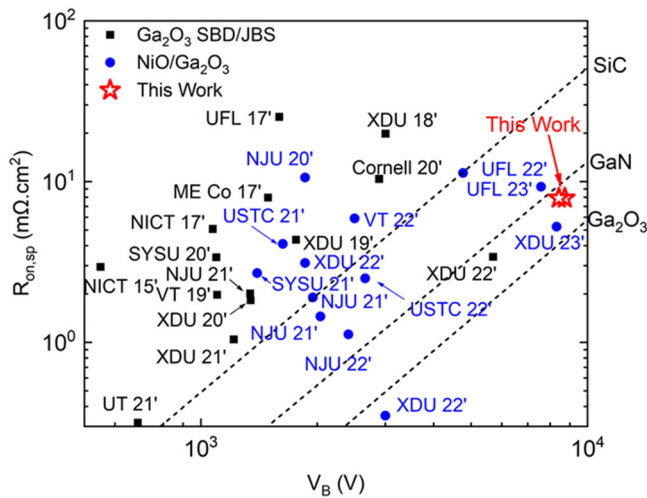


FIG. 11. Compilation of R_{on} vs V_B of conventional and NiO/Ga₂O₃ heterojunction small area rectifiers reported in the literature.

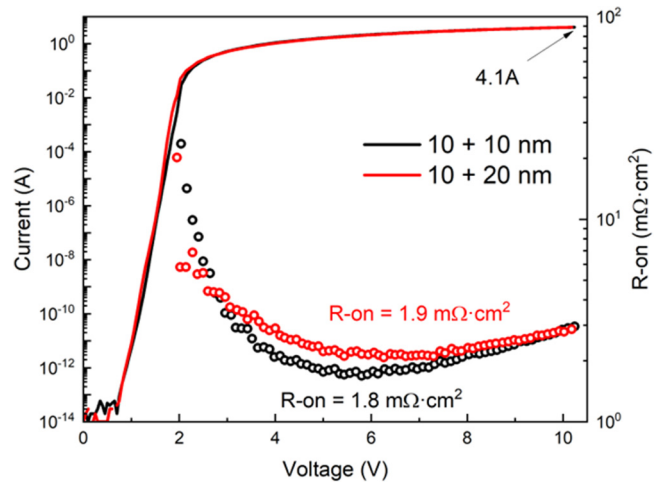


FIG. 12. Forward current characteristics for 1 mm² heterojunction rectifiers for two different NiO thicknesses.

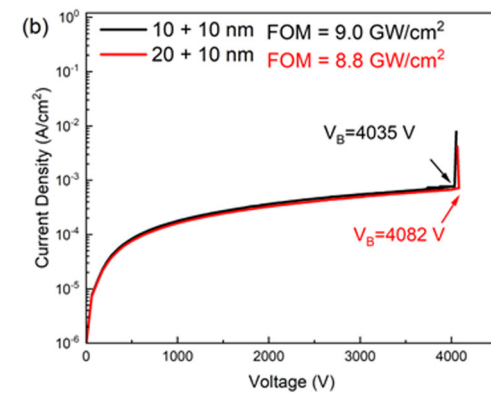
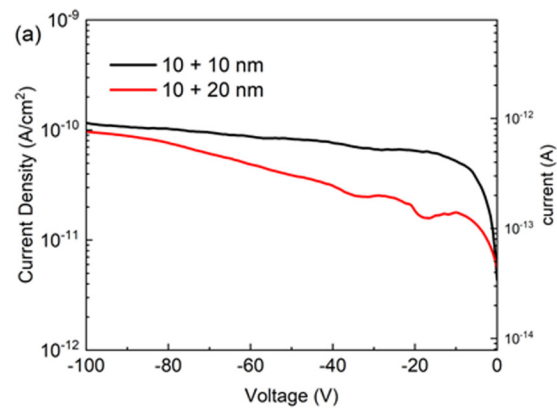


FIG. 13. Reverse J-V characteristics out to (a) -100 V for NiO/Ga₂O₃ rectifiers with 10/10 nm 10/20 nm NiO bilayers. (b) Over full bias range to show V_B .

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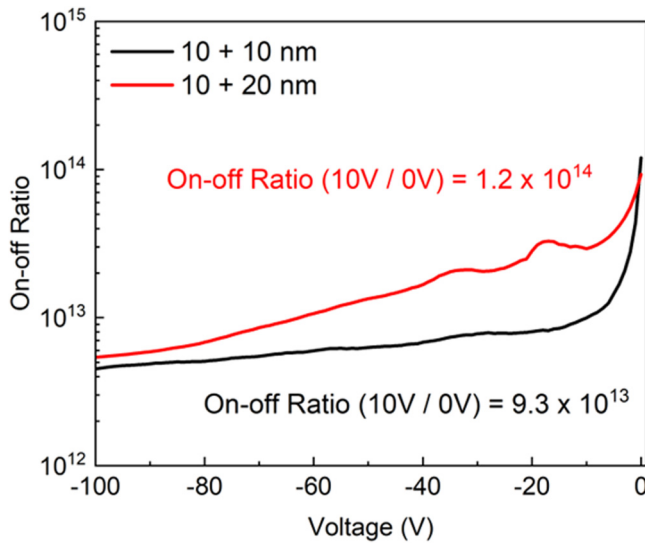


FIG. 14. On-off ratio of 1 mm² NiO/Ga₂O₃ heterojunction rectifiers in which the bias was switched from 5 V forward to the voltage shown on the x axis.

Ampere-class power devices. A recent review has discussed switching performance, packaging, and approaches to thermal management.⁴⁶

We fabricated 1 mm² devices with the same structure as shown in Fig. 1. Figure 12 shows the forward J–V characteristics of two such devices with different NiO thicknesses, with a maximum forward current of 4.1 A at 10 V forward bias. The R_{ON} values are 1.8–1.9 mΩ cm⁻². While rectifier arrays have achieved currents in the range of 33–100 A, 4 A for an individual device is still behind

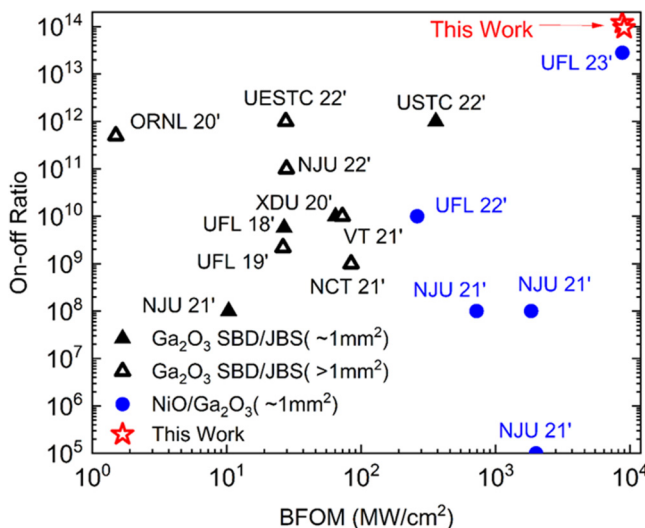


FIG. 15. Compilation of on-off ratio vs power figure of merit of conventional and NiO/Ga₂O₃ heterojunction rectifiers reported in the literature.

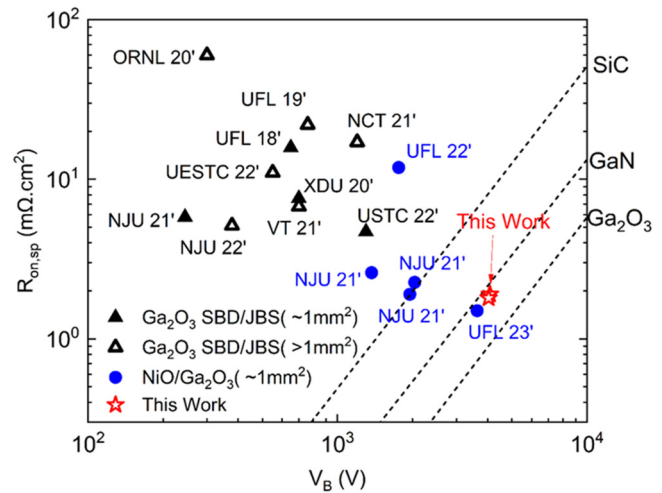


FIG. 16. Compilation of Ron vs V_B of large area conventional and NiO/Ga₂O₃ heterojunction rectifiers reported in the literature.

those of Gong *et al.*⁴⁷ and Zhou *et al.*,⁵¹ where 12 A was achieved. Large area packaged Ga₂O₃ SBDs with an anode size of 3 × 3 mm² have been reported with forward current of over 15 A.⁵⁵

The reverse J–V characteristics are shown in Fig. 13 for two different types of structure with varying NiO thickness. Figure 13 (a) shows the low voltage (–100 V) range, while (b) shows that the V_B values are around 4 kV. These are the highest reported for Ampere-class Ga₂O₃ rectifiers. Once again, the NiO thickness does not have a significant impact on the magnitude of the breakdown voltage.

Figure 14 shows the on-off ratio of 1 mm² NiO/Ga₂O₃ heterojunction rectifiers in which the bias was switched from 5 V forward to the voltage shown on the x axis. The on-off ratio is >10¹² over the whole bias range investigated and is slightly better for the thicker NiO layers. For switching from 10 to 0 V, the ratio is ~10¹⁴ in both cases and these large area devices retain excellent rectification, showing that the increased likelihood of having defects within the active area have not degraded this property. Sdoeung *et al.*⁶⁴ reported that threading dislocations in HVPE layers of the type we are using are responsible for significant contributions to reverse leakage current in rectifiers. Figure 15 shows a compilation of on-off ratio versus power figure of merit of conventional and NiO/Ga₂O₃ heterojunction rectifiers reported in the literature.

Figure 16 shows a compilation of Ron versus V_B of large area conventional and NiO/Ga₂O₃ heterojunction rectifiers reported in the literature. Our results represent the best combination of breakdown voltage and on-state resistance reported to date and show the impressive advances in material quality in terms of reducing both background carrier density and extended defect density.

IV. SUMMARY AND CONCLUSIONS

In summary, we optimized the NiO bilayer thickness and extension of these layers beyond the cathode contact on

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NiO/ β -Ga₂O₃ p-n heterojunction rectifiers to achieve V_B 8.9 kV with R_{on} of 7.9 m Ω cm² and a resultant figure-of-merit (V_B^2/R_{on}) of 10.2 GW cm⁻². The heterojunction produces breakdown voltages far more than Schottky rectifiers fabricated on the same wafer and confirms that the NiO can act as both p-layer and guard ring material. This approach now consistently produces power figure of merits that exceed the unipolar power device performance of both GaN and SiC. It will still be necessary to establish the long-term reliability of devices fabricated by this approach. For large area devices, the low thermal conductivity limitations of Ga₂O₃ remain as a primary issue. In addition, more work is needed to understand the surge current capability of Ga₂O₃-based rectifiers and the packaging approaches needed to achieve practical operating characteristics, along with establishing the junction-to-ambient thermal resistance of junction side cooling approaches.^{65,66}

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AUTHOR DECLARATIONS

Conflict of Interest

The authors have no conflicts to disclose.

Author Contributions

Jian-Sian Li: Data curation (equal); Formal analysis (equal); Investigation (equal); Methodology (equal); Writing – original draft (equal). **Chao-Ching Chiang:** Data curation (equal); Investigation (equal); Methodology (equal); Writing – original draft (equal). **Xinyi Xia:** Conceptualization (equal); Data curation (equal); Investigation (equal); Methodology (equal); Writing – original draft (equal). **Hsiao-Hsuan Wan:** Data curation (equal); Investigation (equal); Methodology (equal); Writing – original draft (equal). **Fan Ren:** Conceptualization (equal); Data curation (equal); Formal analysis (equal); Funding acquisition (equal); Investigation (equal); Methodology (equal); Project administration (equal); Writing – original draft (equal). **S. J. Pearton:** Conceptualization (equal); Data curation (equal); Formal analysis (equal); Funding acquisition (equal); Writing – original draft (equal).

DATA AVAILABILITY

The data that support the findings of this study are available within the article.

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